# About the Presenter

PCA

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- Paul Tennis is the Director of Product Standards and Technology for the Portland Cement Association (PCA).
- Paul has been with PCA in various capacities for 24 years, focused on cement and concrete standards development, including ASTM and AASHTO cement specifications and concrete durability-related standards.
- He holds a Bachelor of Science degree in Ceramic Engineering from Clemson University, and an MS and PhD in Materials Science and Civil Engineering both from Northwestern University.
- He is a fellow of ACI, an ASTM Bryant Mather award recipient, past chairman of ASTM Committee C01, and 'friend' of several AASHTO and TRB committees.
- Fun fact: Paul attended the inaugural meeting of the Midwest Concrete Consortium in 1997 and has participated periodically in the MC2 and NC2 meetings ever since.

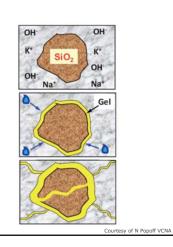


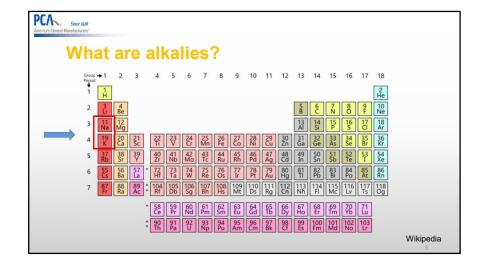


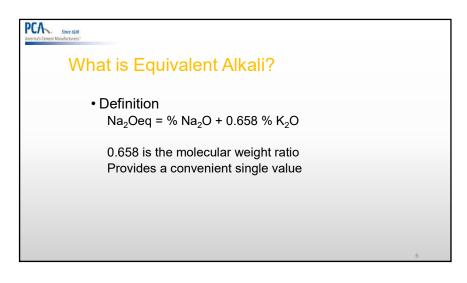


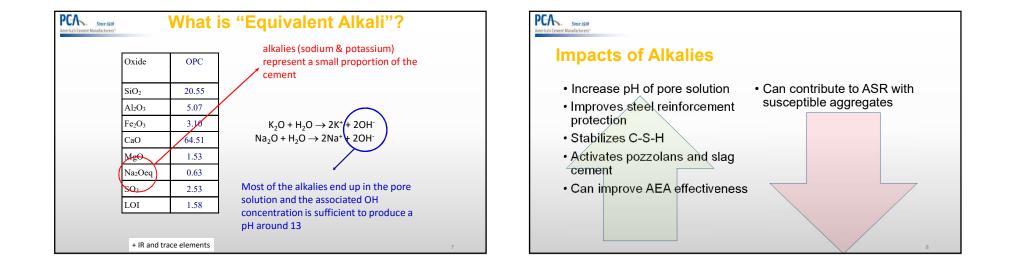
## A little more on ASR...

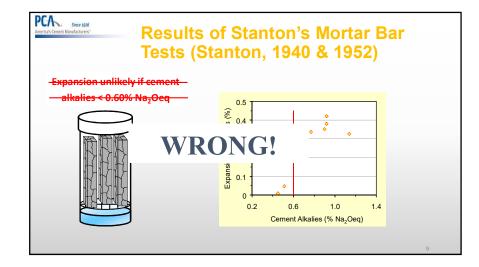
- Aggregates react with soluble alkalies in pore solution with silica in aggregate
- Alkali-Silica gel forms.
- AS Gel fills pores
- Reaction continues

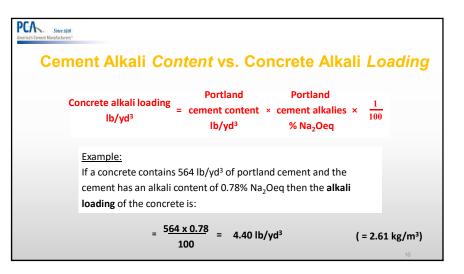


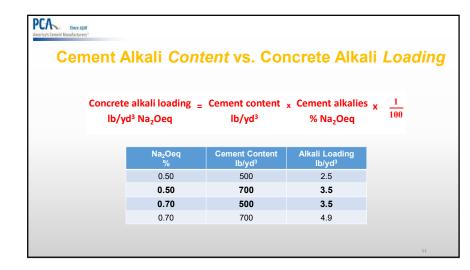


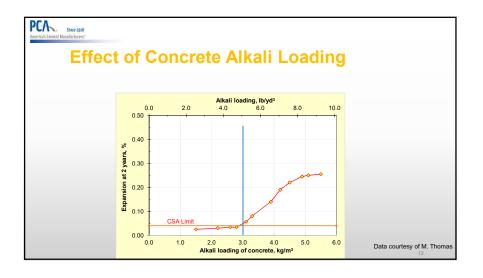












## PCA. Since 1916

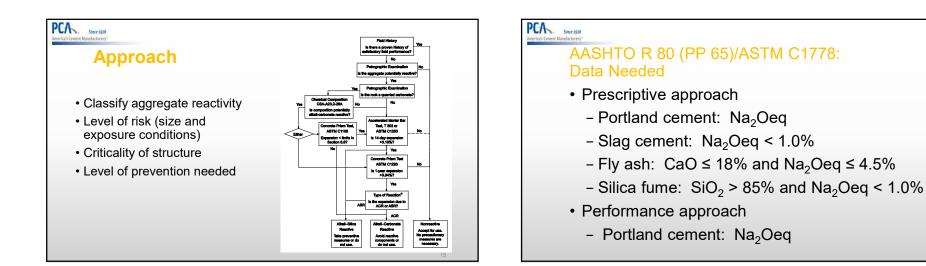
## What changed in the Specs?

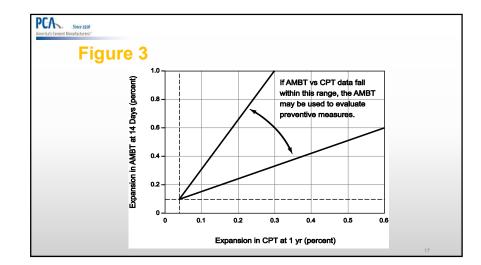
- C150/M 85 no longer include the optional low-alkali limit of 0.60%
- Manufacturers are required to report Na<sub>2</sub>Oeq on all portland cement mill test reports
- Note references ASTM C1778/AASHTO R 80 for guidance on ASR
- Reference to the historical optional limit is included in a nonmandatory note

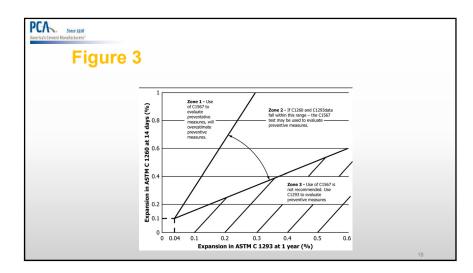
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# Why the Spec Change?

- A 0.60% limit on *cement* is not protective in all cases
  - · False sense of security
  - Aggregate reactivity
  - Concrete mix design
- Alkali loading of *concrete* is more relevant/effective
   Reporting equivalent alkalies allows alkali loading to be readily calculated
- SCMs are most common solution
- C1778 and R 80 provide state-of-the-art guidance







| Table 1. Classification of Aggregate |   |                                  |                                   |  |  |
|--------------------------------------|---|----------------------------------|-----------------------------------|--|--|
| Aggregate-<br>Reactivity<br>Class    | Description of<br>Aggregate<br>Reactivity | 1-Year<br>Expansion in<br>CPT, % | 14-Day<br>Expansion in<br>AMBT, % |  |  |
| R0                                   | Nonreactive                               | ≤0.04                            | ≤0.10                             |  |  |
| R1                                   | Moderately<br>reactive                    | >0.04, ≤0.12                     | >0.10, ≤0.30                      |  |  |
| R2                                   | Highly reactive                           | >0.12, ≤0.24                     | >0.30, ≤0.45                      |  |  |
| R3                                   | Very highly<br>reactive                   | >0.24                            | >0.45                             |  |  |

|  | Aggregate-Reactivity Class |               |                |            |
|--|----------------------------|---------------|----------------|------------|
| Size and Exposure Conditions   | R0                         | R1            | R2             | R3         |
| Nonmassive concrete <sup>a</sup> in a dry environment  | Level 1                    | Level 1       | Level 2        | Level 3    |
| Massive elements <sup>a</sup> in a dry environment   | Level 1                    | Level 2       | Level 3        | Level 4    |
| All concrete exposed to humid air, buried or<br>immersed   | Level 1                    | Level 3       | Level 4        | Level 5    |
| All concrete exposed to alkalies in service <sup>c</sup>   | Level 1                    | Level 4       | Level 5        | Level 6    |
| <ul> <li><sup>a</sup> A massive element has a least dimension &gt;0.9 m (3 ft).</li> <li><sup>b</sup> A dry environment corresponds to an average ambient relati<br/>in buildings.</li> <li><sup>c</sup> Examples of structures exposed to alkalies (sodium and pota<br/>seawater and highway structures exposed to deicing salts (e.<br/>potassium formate, sodium acetate, sodium formate, etc.).</li> </ul> | ssium) in servic           | e include mar | ine structures | exposed to |

| Sev   | erity of Con   | sequences of                                     | ASR   |
|-------|--|--|---|
|       |  |  | AUN   |
| Class | Consequences of ASR                                  | Acceptability of ASR                             | Examples <sup>b</sup>                         |
| S1    | Safety, economic, or<br>environmental consequences   | Some deterioration from ASR may<br>be tolerated. | Non-load-bearing elements inside<br>buildings |
|       | small or negligible                                  |  | Temporary structures (e.g., <5 years)         |
| S2    | Some safety, economic, or                            | Moderate risk of ASR is acceptable.              | Sidewalks, curbs, and gutters                 |
|       | environmental consequences<br>if major deterioration |  | Service life <40 years                        |
| S3    | Significant safety, economic,                        | Minor risk of ASR acceptable.                    | Pavements                                     |
|       | or environmental                                     |  | Culverts                                      |
|       | consequences if minor                                |  | Highway barriers                              |
|       | damage   |  | Rural, low-volume bridges                     |
|       |  |  | Large numbers of precast elements where       |
|       |  |  | economic costs of replacement are sever       |
|       |  |  | Service life normally 40 to 75 years          |
| S4    | Serious safety, economic, or                         | ASR cannot be tolerated.                         | Major bridges                                 |
|       | environmental consequences                           |  | Tunnels                                       |
|       | if minor damage                                      |  | Critical elements that are very difficult to  |
|       |  |  | inspect or repair                             |
|       |  |  | Service life normally >75 years               |

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# Table 3. Level of Prevention

| Level of ASR Risk  | Classification of Structure (Table 4) |    |    |                     |  |
|--|---------------------------------------|----|----|---------------------|--|
| (Table 2)  | S1                                    | S2 | S3 | S4                  |  |
| Risk level 1   | V                                     | V  | V  | V                   |  |
| Risk level 2   | V                                     | V  | W  | Х                   |  |
| Risk level 3   | V                                     | W  | Х  | Y                   |  |
| Risk level 4   | W                                     | Х  | Y  | Z                   |  |
| Risk level 5   | Х                                     | Y  | Z  | ZZ                  |  |
| Risk level 6   | Y                                     | Z  | ZZ | а                   |  |
| <sup>a</sup> It is not permitted to construct a Class S4 structur<br>level of risk in these circumstances. The levels of |                                       |    |    | taken to reduce the |  |

# PCA. Since 1916 America's Cement Manufacturers" Table 5. Maximum Alkali Contents in **Portland Cement Concrete**

#### Maximum Alkali Loading of Concrete (Na<sub>2</sub>Oeq)

| Prevention Level                                    | kg/m³     | lb/yd <sup>3</sup> |    |
|---|-----------|--------------------|----|
| V   | No limit  | No limit           |    |
| W   | 3.0       | 5.0                |    |
| Х   | 2.4       | 4.0                |    |
| Y   | 1.8       | 3.0                |    |
| Za  | Table 8   | Table 8            |    |
| ZZ <sup>a</sup>                                     | Table 8   | Table 8            |    |
|   |           |                    |    |
| <sup>a</sup> SCMs must be used in prevention levels | Z and ZZ. |                    | 23 |

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## **Table 6. Minimum SCM Levels**

|                          | Alkali Level of SCM,    | Minimu  |         | ement Leventitious Ma |         | lass of  |
|--------------------------|-------------------------|---------|---------|-----------------------|---------|----------|
| Type of SCM <sup>a</sup> | (% Na <sub>2</sub> Oeq) | Level W | Level X | Level Y               | Level Z | Level ZZ |
| Fly ash                  | ≤3.0                    | 15      | 20      | 25                    | 35      |          |
| (CaO ≤18%)               | >3.0, ≤4.5              | 20      | 25      | 30                    | 40      |          |
| Slag                     | ≤1.0                    | 25      | 35      | 50                    | 65      |          |
| Silica fume <sup>c</sup> | ≤1.0                    | 2.0 ×   | 2.5 ×   | 3.0 ×                 | 4.0 ×   | Table 8  |
| (SiO <sub>2</sub> ≥85%)  |                         | KGA     | KGA     | KGA                   | KGA     | Table o  |
|                          |                         | or      | or      | or                    | or      |          |
|                          |                         | 1.2 ×   | 1.5 ×   | 1.8 ×                 | 2.4 ×   |          |
|                          |                         | LBA     | LBA     | LBA                   | LBA     |          |
|                          |                         |         |         |                       |         |          |
|                          |                         |         |         |                       |         | 24       |

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# Table 7. Adjustment for Alkali Level ofPortland Cement

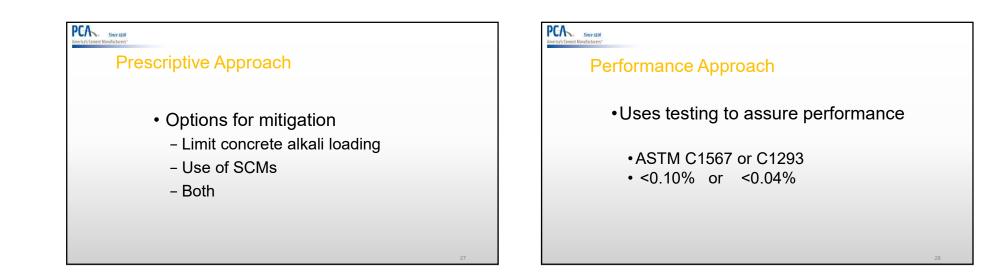
| Cement alkalies         |   |
|-------------------------|---|
| (% Na <sub>2</sub> Oeq) | Level of SCM  |
| ≤0.70                   | Reduce the minimum amount of SCM given in Table 6 by one prevention level. <sup>a</sup> |
| >0.70, ≤1.00            | Use the minimum levels of SCM given in Table 6.   |
| >1.00, ≤1.25            | Increase the minimum amount of SCM given in Table 6 by one prevention level.            |
| >1.25                   | No guidance is given.   |

<sup>a</sup> The replacement levels should not be below those given in Table 6 for prevention level W, regardless of the alkali content of the portland cement.

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# Table 8. Using SCM and Limiting Alkali Contentto Provide Exceptional Levels of Prevention

|                     | SCM as Sole<br>Prevention                 | Limiting Concrete Alk   | kali Loading Plus SCM                     |  |
|---------------------|---|---|---|--|
| Prevention<br>Level | Minimum SCM Level                         | Maximum Alkali<br>Loading, kg/m <sup>3</sup><br>(lb/yd <sup>3</sup> ) | Minimum SCM Level                         |  |
| Z                   | SCM level shown for<br>Level Z in Table 6 | 1.8 (3.0)   | SCM level shown for<br>Level Y in Table 6 |  |
| ZZ                  | Not permitted                             | 1.8 (3.0)   | SCM level shown for<br>Level Z in Table 6 |  |



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#### Performance approach: Data Needed

- C1293: Adjusts mix water alkali content based on portland cement
- Equivalent alkali content of portland cement or portland cement portion of blended cement

# **Conclusion**Alkali-Silica Reactivity (ASR) Alkalies in Cement and Concrete Cement equivalent alkali content Concrete alkali loading Benefits of alkalies in concrete ASTM C1778/AASHTO R 80 for best guidance now and for the future http://mdot.mse.mtu.edu/dotspecs/